

Studies on Lattice Calibration With Frequency Analysis of Betatron Motion

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• Outline:

***Introduction**

- NAFF
- perturbative theory of betatron motion
- SVD fit of lattice parameters

DIAMOND Spectral Lines Analysis

- Linear Model
- Nonlinear Model





- Closed Orbit Response Matrix (LOCO-like)
- Frequency Map Analysis
- Frequency Analysis of Betatron Motion (resonant driving terms)





Define the distance between the two vector of Fourier coefficients

$$\chi^{2} = \sum_{k} \left(A_{Model}(j) - A_{Measured}(j) \right)^{2}$$

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Least Square Fit (SVD) of accelerator parameters θ

to minimize the distance χ^2 of the two Fourier coefficients vectors

- Compute the "Sensitivity Matrix" M
- Use SVD to invert the matrix M
- Get the fitted parameters

 $\Delta \overline{A} = M\overline{\theta}$ $M = U^T W V$ $\overline{\theta} = (V^T W^{-1} U) \Delta \overline{A}$

$\text{MODEL} \rightarrow \text{TRACKING} \rightarrow \text{NAFF} \rightarrow$

Define the vector of Fourier Coefficients – Define the parameters to be fitted $SVD \rightarrow CALIBRATED MODEL$



Main parameters:

100 MeV Linac

3 GeV Booster (158.4 m)

3 GeV Storage Ring (561.6 m)

24 cell DBA lattice2 + 1 SC RF cavities18 straight for ID (5

m)

6 long straights (8 m)



Commissioning end 2006





Measurement of Resonant driving terms of non linear resonances



The quasi periodic decomposition of the orbit

$$x(n) - ip_x(n) = \sum_{k=1}^n c_k e^{2\pi i v_k n}$$
 $c_k = a_k e^{i\phi_k}$

can be compared to the perturbative expansion of the non linear betatron motion

$$x(n) - ip_{x}(n) = \sqrt{2I_{x}}e^{i(2\pi Q_{x}n + \psi_{0})} + -2i\sum_{jklm} js_{jklm}(2I_{x})^{\frac{j+k-1}{2}}(2I_{y})^{\frac{l+m}{2}}e^{i\left[(1-j+k)(2\pi Q_{x}n + \psi_{x0}) + (m-l)(2\pi Q_{y}n + \psi_{y0})\right]}$$

Each resonance driving term s_{jklm} contributes to the Fourier coefficient of a well precise spectral line

$$v(s_{jklm}) = (1 - j + k)Q_x + (m - l)Q_y$$

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Spectral Lines detected with NAFF algorithm

e.g. Horizontal:

• (1, 0)	1.10 10-3	horizontal tune
• (0, 2)	1.04 10-6	$Q_x - 2 Q_z$
• (-3, 0)	2.21 10-7	4 Q _x
• (-1, 2)	1.31 10-7	$2 Q_x + 2 Q_z$
• (-2, 0)	9.90 10-8	3 Q _x
• (-1, 4)	2.08 10-8	$2 Q_x + 4 Q_z$

Longitudinal Variation of Driving Terms





 \Rightarrow Amplitude of Driving Terms not the same \Rightarrow Amplitude constant between lattice errors

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Linear Coupling in SPS











The resonance (3,0) introduces the spectral Change polarities of the extraction sextupoles? line (-2,0).



 \Rightarrow We have a problem!

Hardware checks confirmed that these sextupoles had opposite polarities.

Sextupole Driving Terms with Extraction Sext.



Extraction Sextupoles powered to ++++---30 A. Data fully decohered \Rightarrow Line reduced by a factor 2.



 \Rightarrow Large discrepancies: We have a problem!

The closed orbit as measured from pick-ups is introduced at the extraction sextupoles in the model.



 \Rightarrow Improvement due to beta–beating and phase differences in the model.



 β_{v} function vs BPM position

S (m

(1, 0) Line Amplitude vs BPM position

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(-2, 0) spectral line: resonance driving term h_{3000} (3Q_x = p) at all BPMs Main spectral line (Tune Q_{y})



- The amplitude of the tune spectral line replicates the β functions
- The amplitude of the (-2, 0) show that third order resonance is well compensated within one superperiod. Some residual is left every two cells ($5\pi/2$ phase advance)

Amplitude of Spectral Lines for low emittance DIAMOND lattice computed at all the BPMs



The coupled linear motion in each plane can be written in terms of the coupling matrix

$$C = \begin{pmatrix} c_{11} & c_{12} \\ c_{21} & c_{22} \end{pmatrix}$$

e.g. for the horizontal motion

 $\begin{aligned} \zeta_{x} &= x - ip_{x} = a_{1}e^{i(\phi_{u} + \delta_{u})} + a_{2}e^{-i(\phi_{u} + \delta_{u})} + \\ &+ a_{3}e^{i(\phi_{v} + \delta_{v})} + a_{4}e^{-i(\phi_{v} + \delta_{v})} \end{aligned}$

 a_3 and a_4 depend linearly on c_{ij}

- two frequencies (the H tune and V tune)
- no detuning with amplitude



0.1 mrad kick in both planes

(0,1) spectral line for low emittance DIAMOND lattice computed at all the second distributes (V misalignment errors added to chromatic sextupoles) $h_{1001p} = \frac{1}{2\pi} \int_{-\infty}^{2\pi R} a_2(s) \left(\frac{\beta_x}{2}\right)^{1/2} \left(\frac{\beta_z}{2}\right)^{1/2} e^{i(W_x(s) - W_z(s)) - i\frac{ps}{R}} ds$ The resonance driving term h_{1001} contributes to the (0, 1) spectral line in



The amplitude of the (0, 1) spectral line replicates well the s dependence of the difference resonance $Q_x - Q_z$ driving term



DIAMOND Spectral Lines Analysis

* Horizontal Misalignment of sextupoles (β – beating)
* Vertical Misalignment of sextupoles (linear coupling)
* Gradient errors in sextupoles (non linear resonances)



The generated normal quadrupole components introduce a β - beating.

• we build the vector of Fourier coefficients of the horizontal and vertical tune line





We build the vector $\overline{A} = (a_1^{H(1,0)} \dots a_{NBPM}^{H(1,0)} a_1^{V(0,1)} \dots a_{NBPM}^{V(0,1)})$ containing the amplitude of the tune lines in the two planes at all BPMs $\chi^{2} = \sum_{j} \left(A_{Model}(j) - A_{Measured}(j) \right)^{2}$ We minimize the sum 1.6 ~ 10[~] 1.4 1.2 1.5 0.8 0.6 0.4 0.5 0.2 25 3.5 15 χ^2 as a function of the iteration number Example of SVD principal values

Fitted values for the 24 horizontal sextupole misalignments obtained from the SVD





Fitted values for the 72 horizontal sextupole misalignments obtained from the SVD





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The generated skew quadrupole components introduce a linear coupling.

- we build the vector of Fourier coefficients of the (0, 1) line in the H plane
- we use the vertical misalignments as fit parameters





We build the vector $\overline{A} = (a_1^{H(0,1)} \dots a_{NBPM}^{H(0,1)} \phi_1^{H(0,1)} \dots \phi_{NBPM}^{H(0,1)})$ containing the amplitude and phase of the (0, 1) line in the H planes at all BPMs



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Fitted values for the 24 vertical sextupole misalignments obtained from SVD





Fitted values for the 72 vertical sextupole misalignments obtained from SVD







The sextupole gradient errors spoil the compensation of the third order resonances, e.g $3Q_x = p$ and $Q_x - 2Q_z = p$

- we build the vector of Fourier coefficients of the H(-2,0) and H(0,2) line
- we use the errors gradients as fit parameters





We build the vector
$$\overline{A} = (a_1^{H(-2,0)} \dots a_{NBPM}^{H(-2,0)} a_1^{H(0,2)} \dots a_{NBPM}^{H(0,2)})$$

containing the amplitudes at all BPMs

- the (-2, 0) line in the H plane related to h_{3000}
- the (0, 2) line in the H plane related to h_{1002}

We minimize the sum

$$\chi^{2} = \sum_{j} \left(A_{Model}(j) - A_{Measured}(j) \right)^{2}$$



 χ^2 as a function of the iteration number





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ALS example (very early results)









 Resonance driving term analysis provides quantitative information about nolinearities in the machine

• It allows to measure the local distribution of the dominant nonlinearities

• However, it does not give a direct information about how harmful the nonlinearities are

• Theoretically it can provide a method similar to orbit response matrix analysis (or phase advance, ...) to measure not just the gradient and skew gradient distribution, but also the setxupole, (octupole), ... How well this will work experimentally is not quite clear, yet:

•Can we use the spectral lines to recover the LINEAR and NON LINEAR machine model with a Least Square method?

• SPS with a few very large nonlinearities worked well. Diamond simulations look encouraging. ALS measurements so far seem BPM resolution limited.



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