

## Comparison of Booster ring "Bump magnet" B field measurements vs. calculations @ 1.552 and 1.995 Gev.

### Bump magnet measurements on 4/9/04:

#### - Equipment used:

a) **Gauss meter and sensor:** The model YR100-3-2 is a self contained, high linearity, high stability magnetic field to analog voltage transducer for one component of a magnetic field. It is particularly appropriate for magnetic fields up to 2T with better than 0.1% absolute accuracy at 1T and with a frequency response from dc to 10kHz. Probe is guaranteed flat to 1.0 KHz

b) **Magnet current sensor:** Pearson 101 current probe

c) **Monitor scope:** TDS5000 digital oscilloscope

#### Measurement data:

Gmeter	Bmeter (gauss)	Ipeak - DSO	Bcalc	Icalc
1	4000	238	3670	238
1.07	4280	260		
1.16	4640	280		
1.2	4800	290		
1.24	4960	298		
1.28	5120	308	4720	306
1.32	5280	312		

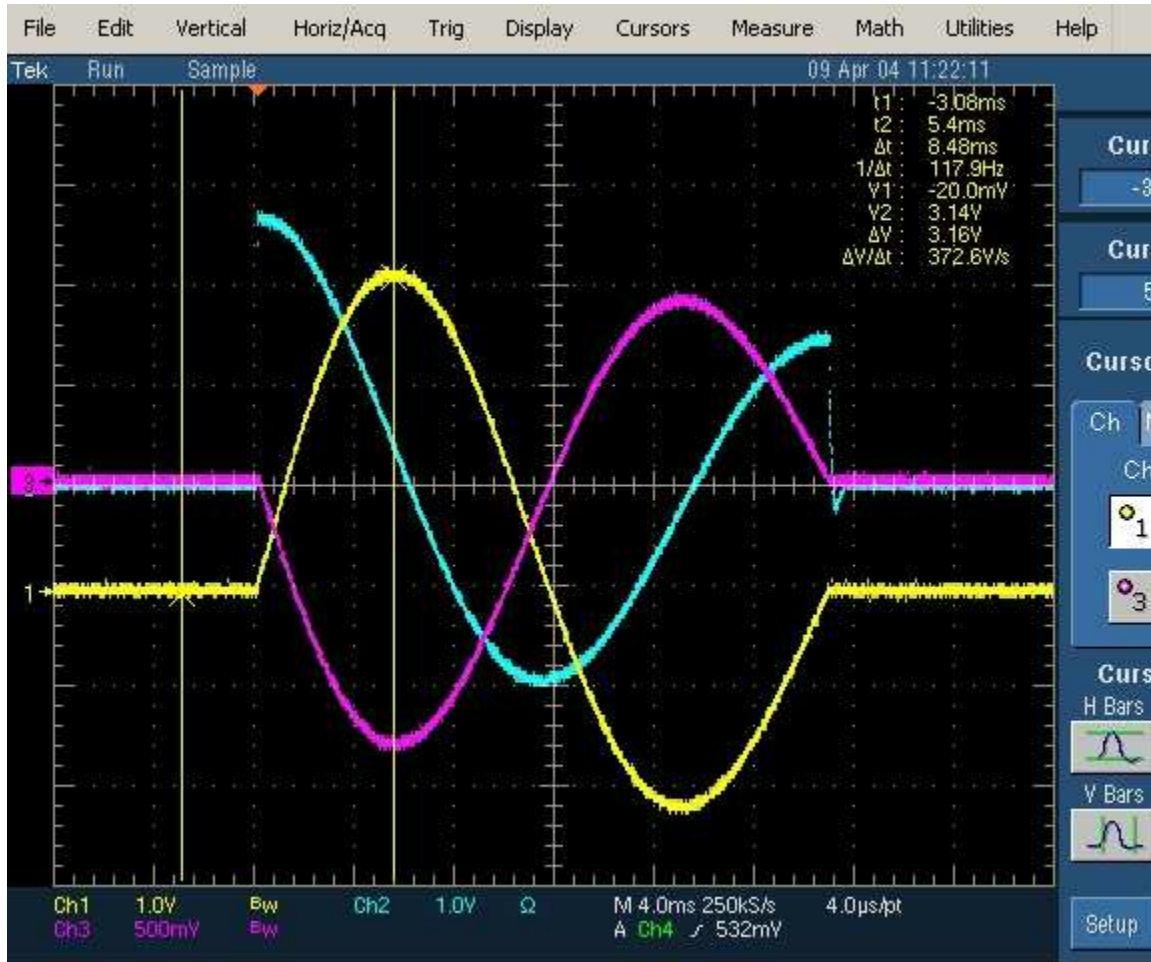
#### Notes:

- 1) Pulse to pulse current variations not shown in data. Was roughly +/- 1.5%
- 2) Pulse to pulse B field variations not shown in data. Was roughly +/- 1.7%
- 3) Variations included in error bar data included in graph below.

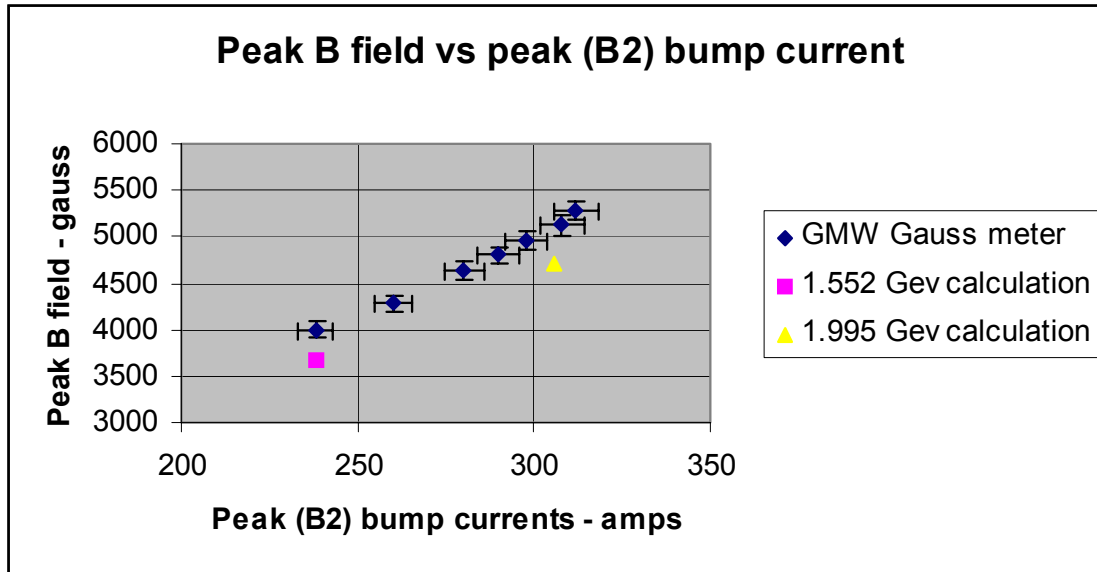
Waveform pictures taken at peak drive current of 312 amps.

Color code:

- Yellow is magnet current @ 100 amp/volt - value measured by pair cursors.
- Turquoise is applied voltage @ 100 volts/volt
- Purple is B field measured with Hall element @ 4000 gauss/volt



**Plotted data:**



**Key notes results observed:**

- 1) Only central bump magnet (B2) was measured for following reasons:
  - a) Center axis of magnet above the beam tube most easily accessed by Hall probe
  - b) From calculations below B2 has the highest current requirements.
- 2) Theoretical data points for 1.552 and 1.995 are colored square and triangle. Calculated results are derived below
- 3) **Measurement anomaly: Off axis (from beam center line) B field measurements increased linearly up to approximately  $1.5 \times 5280 = 7920$  gauss.**

**Theoretical calculations:**

- 1) Key numeric results enclosed in rectangular borders
- 2) Key facts or conclusions in Bold and Blue.
- 3) Data for calculations from Engineering note AL0323, M4852, 6/20/89

**Global variable assignments:**

$$\text{Gev} \equiv 1 \cdot 10^9 \cdot \text{volt} \quad \text{KV} \equiv 10^3 \quad \text{mrad} \equiv 10^{-3} \quad \text{mm} \equiv 10^{-3} \cdot \text{m} \quad \mu \equiv 10^{-6}$$

$$\text{ms} \equiv 10^{-3} \cdot \text{sec} \quad \mu_0 \equiv 4 \cdot \pi \cdot 10^{-7} \cdot \frac{\text{henry}}{\text{m}} \quad \text{m}\Omega \equiv 10^{-3} \cdot \text{ohm} \quad \text{K} \equiv 10^3$$

**Peak B field nominal deflections at 1.552 Gev:**

$B\rho$  = beam stiffness

$$Z := 1 \quad Z = \text{charge} = 1$$

$$E_{1.5} := 1552 \quad \text{Nominal Beam extraction energy in Mev.}$$

$$E_0 := .51 \quad E_0 = \text{electron rest energy}$$

$$L_{\text{eff}} := 0.129 \cdot \text{m} \quad \text{Effective length from (note 1) derived from POISSON using variable permeability steel - **This may change due to saturation and end effects**}$$

$$B\rho := \frac{1 \left( E_{1.5}^2 + 2 \cdot E_{1.5} \cdot E_0 \right)^{\frac{1}{2}} \cdot \text{tesla} \cdot \text{m}}{300 \cdot Z}$$

$$B\rho = 5.175 \text{ tesla} \cdot \text{m} \quad \text{Beam rigidity fm. note 1} = 5.00346 \text{ T-M (assumes 1500 Gev but we actually inject at 1.552 Gev.)}$$

$$B \cdot L_{\text{eff}} := B\rho \cdot \theta^2 \quad \text{And}$$

$$\theta_i := \frac{(B \cdot L_{\text{eff}})^{\frac{1}{2}}}{B\rho} \quad \text{To find theta we need to know the peak B field which is defined by the peak current values measured during the standard injection operation.}$$

$$\text{For: } j := 0..2 \quad \text{And: } \eta := .98 \quad N := 84 \quad g := 67 \cdot \text{mm} \quad \mu_0 = 1.257 \times 10^{-6} \frac{\text{henry}}{\text{m}}$$

$$I_{pk_j} :=$$

138 · amp
-238 · amp
93 · amp

**$I_{pk_j}$  (left) are the peak current values for nominal injection energy measured on 3/26/04 for bump magnets B1,2, and 3 respectively.**

**Note: Calculated Currents from note AL0323 for 11mm deflections are: 199, -389, and 152 amps respectively.**

$$B := \frac{I_{pk}}{g} \cdot N \cdot \mu_0 \cdot \eta \quad \text{And:}$$

$$B = \begin{pmatrix} 0.213 \\ -0.367 \\ 0.144 \end{pmatrix} \text{ tesla}$$

Calculated flux densities at 1.552 Gee for for bump magnets B1,2, and 3 respectively. **B2 shown as red square in graph above.**  
 Calculated fields for 11mm deflection from note AL0323 are: .308, -.600, .235 Tesla

**And the calculated angles are 1.552 Gee are:**

$$\theta_i := \frac{(B \cdot L_{eff})}{B\rho}$$

$$\theta_i = \begin{pmatrix} 5.311 \\ -9.16 \\ 3.579 \end{pmatrix} \text{ mrad}$$

Max bend angles for 11mm deflection from Engineering note 1 are 7.95, -15.47, 6.07 mad

**Peak B field nominal deflections at 1.995 Gev:**

$B\rho$  = beam stiffness

$$Z := 1 \quad Z = \text{charge} = 1$$

$$E_{1.9} := 1995 \quad \text{Beam extraction energy in Mev. + 5\% overrange}$$

$$E_0 := .51 \quad E_0 = \text{electron rest energy}$$

$L_{eff} := 0.129 \cdot m$  Effective length from (note 1) derived from POISSON using variable permeability steel - **This will change due to saturation which according to Poisson plots from note AL0323 are still relatively minor at 1.995 Gev**

$$B\rho := \frac{1 \left( E_{1.9}^2 + 2 \cdot E_{1.9} \cdot E_0 \right)^{\frac{1}{2}}}{300 \cdot Z} \cdot \text{tesla} \cdot m$$

$B\rho = 6.652 \text{ tesla}\cdot\text{m}$       Beam rigidity for 1.995 Gev

$B\cdot L_{\text{eff}} := B\rho\cdot\theta$       And

$\theta_i := \frac{(B\cdot L_{\text{eff}})}{B\rho}$

To find theta at 1.995 Gev we need to know the peak B fields which are defined by the peak current values measured during the injection operation. A linear ratio (1.995/1.552) assumes a low core saturation which is confirmed by Poisson plots for 11mm deflection case.

For:       $k := 0..2$

$I_{pk1.9} := \left( \frac{E_{1.9}}{E_{1.5}} \right) \cdot I_{pk}$       And:       $\eta := .98$        $N := 84$        $g := 67\cdot\text{mm}$        $\mu_0 = 1.257 \times 10^{-6} \frac{\text{henry}}{\text{m}}$

$I_{pk1.9} = \begin{pmatrix} 177.39 \\ -305.934 \\ 119.546 \end{pmatrix} \text{ amp}$
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**Peak currents for required deflection at 1.995 Gev**

$B := \frac{(I_{pk1.9})}{g} \cdot N \cdot \mu_0 \cdot \eta$       And:

$B = \begin{pmatrix} 0.274 \\ -0.472 \\ 0.185 \end{pmatrix} \text{ tesla}$
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Calculated flux densities at 1.995 Gev for for bump magnets B1,2, and 3 respectively. **B2 shown as "blue" square in graph above.** Calculated fields for 11mm deflection from AL0323 note are: .308, -.600, .235 Tesla

And the calculated angles are:

$\theta_i := \frac{(B\cdot L_{\text{eff}})}{B\rho}$

$\theta_i = \begin{pmatrix} 5.312 \\ -9.161 \\ 3.58 \end{pmatrix} \text{ mrad}$
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**Max bend angles for 11mm deflection** from AL0323 note are 7.95, -15.47, 6.07 mrad







